

Analysis and Discretization of Time-Domain Impedance Boundary Conditions in Aeroacoustics

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Florian Monteghetti¹, Denis Matignon,² Estelle Piot¹

¹ONERA-DMPE, Université de Toulouse

²ISAE-SUPAERO, Université de Toulouse

Contact: florian.monteghetti@isae.fr



Motivation: noise reduction



Fig. Trent 900 (A380). Inlet lined with a sound absorbing material.

Perforated plate

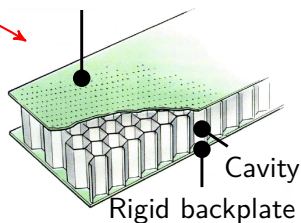


Fig. Example of liner.

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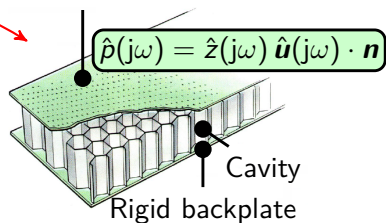


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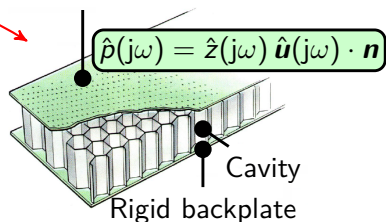


Fig. Example of liner.

Time-harmonic (ω) or time-domain (t) formulation?

Pros of a time-domain formulation (Tam 2012)

- Broadband sources
- Nonlinear PDE (CFD)
- Nonlinear absorption
- + Theoretical interest

⇒ **Objective** Time-domain **impedance** boundary condition (IBC).

Outline

- 1 Introduction
 - Applicability and admissibility of IBCs
 - Existing impedance models
 - Objectives

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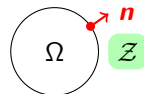
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IBC: Definition, applicability, admissibility

PDE of interest

$$\partial_t \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} + \sum_{i=1}^d A_i \partial_{x_i} \begin{pmatrix} \mathbf{u} \\ p \end{pmatrix} = 0 \quad \text{on } \Omega$$

with IBC on $\partial\Omega$.



Definition of an impedance boundary condition (IBC)

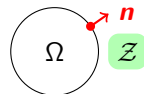
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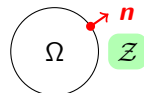
Definition of an impedance boundary condition (IBC)

$$p = \mathcal{Z}(\mathbf{u} \cdot \mathbf{n}) \quad \xrightarrow{\text{LTI}} \quad p(t) = \left[\mathbf{z} \star_t \mathbf{u} \cdot \mathbf{n} \right] (t)$$

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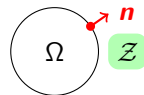
$$\mathbf{u} \cdot \mathbf{n} = \mathcal{Y}(p) \quad \xrightarrow{\text{LTI}} \quad \mathbf{u} \cdot \mathbf{n} = \mathbf{y} \star_t p$$

$$p - \mathbf{u} \cdot \mathbf{n} = \mathcal{B}(p + \mathbf{u} \cdot \mathbf{n}) \quad \xrightarrow{\text{LTI}} \quad p - \mathbf{u} \cdot \mathbf{n} = \beta \star_t (p + \mathbf{u} \cdot \mathbf{n})$$

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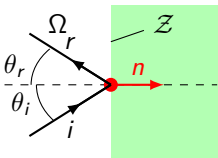
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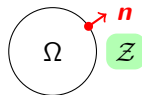
Applicability Only to locally reacting surfaces (Kinsler et al. 1962, §6.7).



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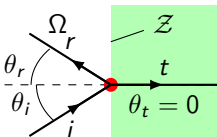
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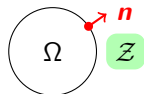
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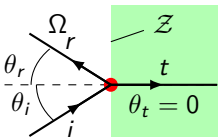
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\Rightarrow An **admissible IBC** dissipates energy at $\partial\Omega$.

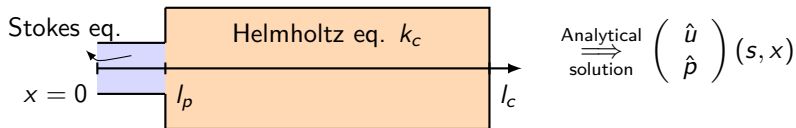
What do impedance models look like ?

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Physical models vs numerical models

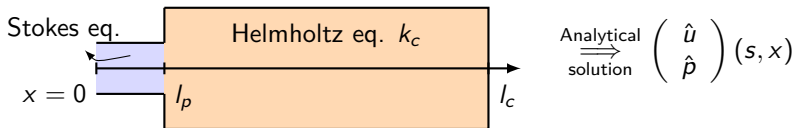
Physical modeling of SDOF liner



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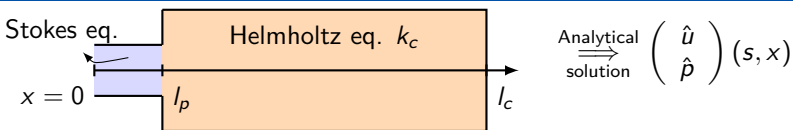


$$\hat{z}_{\text{phys}}(s) = \frac{1}{\sigma_p} \frac{\hat{p}(0)}{\hat{u}(0)} \underset{+\infty}{=} a_0 + a_{1/2} \sqrt{s} + a_1 s + \frac{1}{\sigma_c} \coth(b_0 + b_{1/2} \sqrt{s} + b_1 s)$$

where fractional terms are linked to viscothermal diffusion $a_{1/2}, b_{1/2} \propto \sqrt{\nu}$.

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Early works: (S. Davis 1991), (Tam et al. 1996), (Özyörük et al. 1998).

Common models EHR (Rienstra 2006)

$$\hat{z}_{\text{num}}(s) = a_0 + a_1 s + a_2 \coth(b_0 + b_1 s)$$

⇒ Discretization (Chevaugnon et al. 2006)

Multipole (Fung et al. 2001)

$$\hat{z}_{\text{num}}(s) = \sum_{k=1}^N \frac{r_k}{s - s_k}$$

⇒ "Recursive" convolution

⇒ ODE (Bin et al. 2009)

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Objectives

State of the art

- Physical \neq numerical models
- Numerical models mostly linear
- Admissibility & stability explored by different communities

Objectives

Consider physical, computational, and mathematical aspects of IBCs.

- (a) Time-domain structure of physical impedance models?
- (b) Well-posedness and stability?
- (c) Discretization?
- (d) Nonlinear absorption mechanisms?

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|----------|---|
| Intro | Admissibility and examples of IBCs |
| Part I | Time-domain analysis of physical models |
| Part II | Discontinuous Galerkin discretization |
| Part III | Stability of wave equation |

Part I: objective of model analysis

Objective Time-domain expression of linear physical models \hat{z}_{phys}

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Principle \hat{z}_{phys} can be expressed using two simpler kernels:

Time delay

$$e^{-s\tau}$$

Oscillatory-diffusive (OD)

$$\hat{h}(s)$$

⇒ Enables to deduce discrete model \hat{z}_{num} from \hat{z}_{phys}

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Application to a CT liner impedance model ($z_c, \sigma_c = 1$):

$$\hat{z}_{\text{phys}}(s) = \coth(b_0 + b_{1/2}\sqrt{s} + b_1s) \quad (\Re(s) > 0)$$

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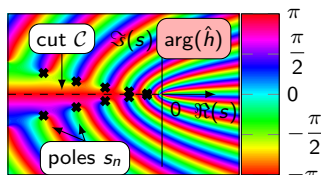
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Oscillatory-diffusive representation

$$\hat{h}(s) = \underbrace{\sum_{k \in \mathbb{Z}} \frac{r_k}{s - s_k}}_{\text{oscillatory part (poles } s_k)} + \underbrace{\int_0^{\infty} \frac{\mu(\xi)}{s + \xi} d\xi}_{\text{diffusive part (cut)}}$$



Outline

- 2 Physical impedance models in the time domain
 - Application to CT impedance model

Application to CT model: realization

Two steps to express $z_{\text{phys}} \star u(t) = u(t) + h \star u(t - \tau)$.

(1) Oscillatory-Diffusive

(2) Delay

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Two steps to express $z_{\text{phys}} \star u(t) = u(t) + h \star u(t - \tau)$.

(1) Oscillatory-Diffusive Convolution expressed with **diffusive variable** φ

$$h \star u(t) = \sum_{k \in \mathbb{Z}} r_k \varphi(t, -s_k) + \int_0^{\infty} \varphi(t, \xi) \mu(\xi) d\xi,$$

which can be computed through first-order **ODEs**

$$\partial_t \varphi(t, x) = -x \varphi(t, x) + u(t), \quad \varphi(t=0, x) = 0 \iff \varphi(t, x) := e^{-xt} \star_t u.$$

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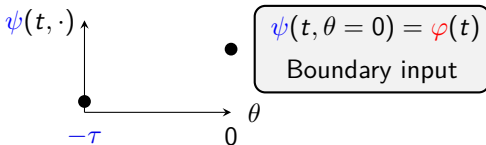
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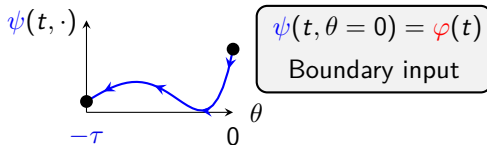
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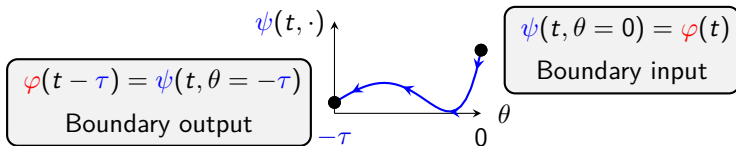
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The representation of \hat{z}_{phys} suggests

$$\hat{z}_{\text{num}}(s) := 1 + e^{-\tau s} \hat{h}_{\text{num}}(s), \quad \hat{h}_{\text{num}}(s) = \sum_{k=1}^{N_s} \frac{r_k}{s - s_k} + \sum_{k=1}^{N_\xi} \frac{\mu_k}{s + \xi_k}$$

Time-local computation of $z_{\text{num}} \star u$ through

PDE ○ ODE, $(N_\psi + 1) \times (N_s + N_\xi)$ variables

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Oscillatory-Diffusive Cost function

$$J(r_k, \mu_k, \xi_k, s_k) = \sum_{k=1}^K |\hat{h}(j\omega_k) - \hat{h}_{\text{num}}(j\omega_k)|^2$$

- ① Choose ξ_k , compute s_k and $r_k = \text{Res}(\hat{h}, s_k)$
- ② Compute $\mu_k = \text{argmin} J(r_k, \cdot, \xi_k, s_k)$
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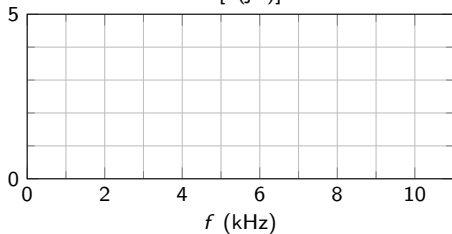
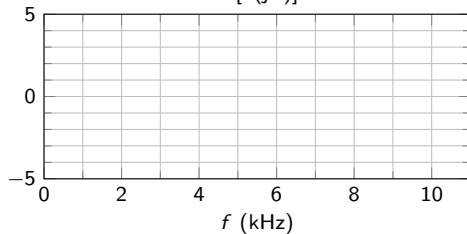
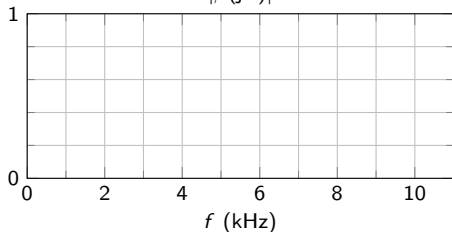
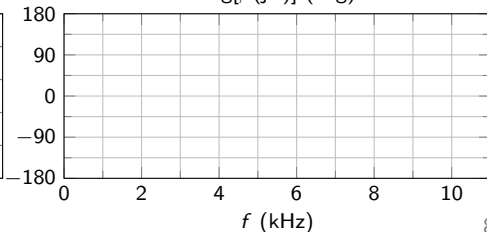
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Delay Discontinuous Galerkin (DG) of order N_ψ on $(-\tau, 0)$

$$\text{PPW}(f) := \frac{N_\psi}{\tau f}$$

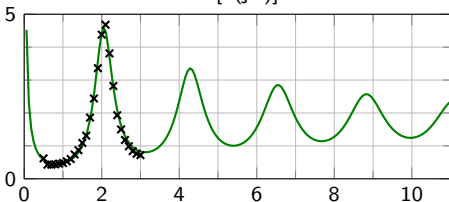
Application to CT model: illustration

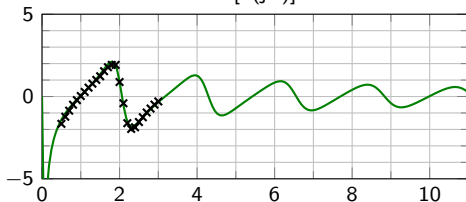
$$\hat{z}_{\text{phys}}(j\omega) \simeq 1 + e^{-\tau j\omega} \left[\sum_{k=1}^{N_s} \frac{r_k}{j\omega - s_k} + \sum_{k=1}^{N_\xi} \frac{\mu_k}{j\omega + \xi_k} \right] =: \hat{z}_{\text{num}}(j\omega)$$

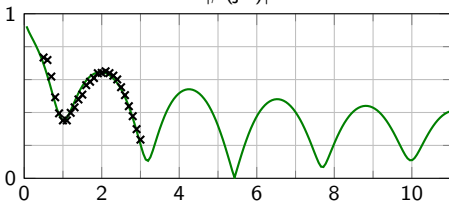
 $\Re[\hat{z}(j\omega)]$  $\Im[\hat{z}(j\omega)]$  $|\hat{\beta}(j\omega)|$  $\text{Arg}[\hat{\beta}(j\omega)]$ (deg)

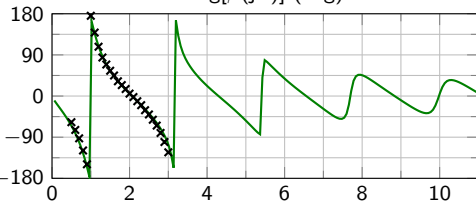
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$$\hat{z}_{\text{phys}}(j\omega) \simeq 1 + e^{-\tau j\omega} \left[\sum_{k=1}^{N_s} \frac{r_k}{j\omega - s_k} + \sum_{k=1}^{N_\xi} \frac{\mu_k}{j\omega + \xi_k} \right] =: \hat{z}_{\text{num}}(j\omega)$$

 $\Re[\hat{z}(j\omega)]$

 f (kHz)

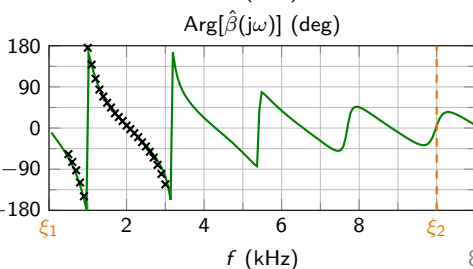
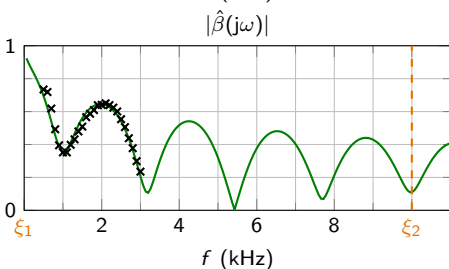
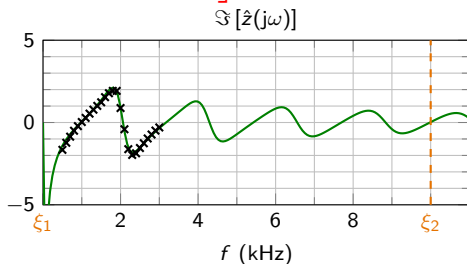
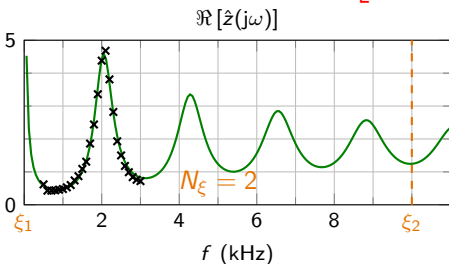
 $\Im[\hat{z}(j\omega)]$

 f (kHz)

 $|\hat{\beta}(j\omega)|$

 f (kHz)

 $\text{Arg}[\hat{\beta}(j\omega)]$ (deg)

 f (kHz)

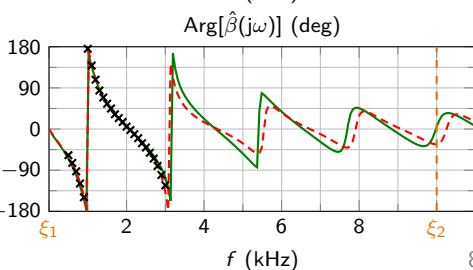
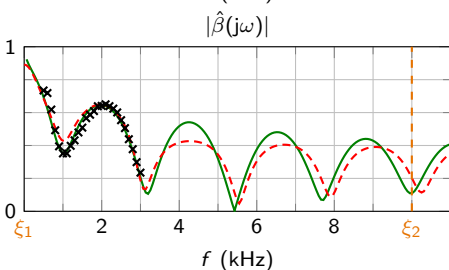
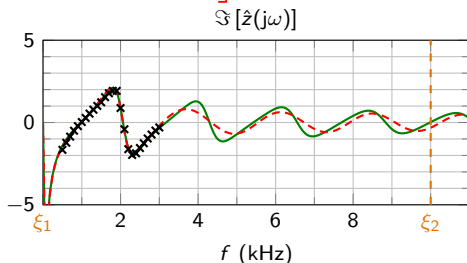
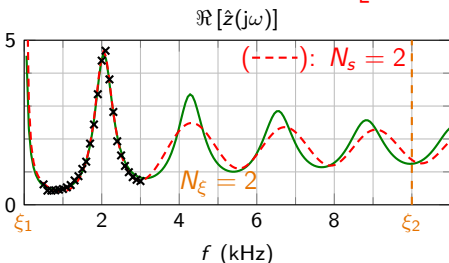
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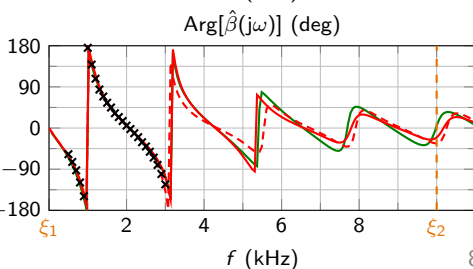
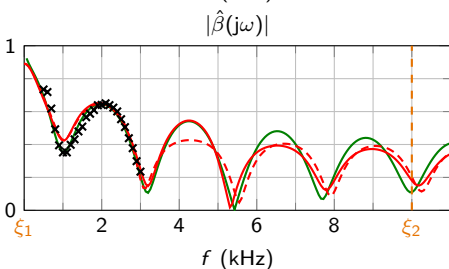
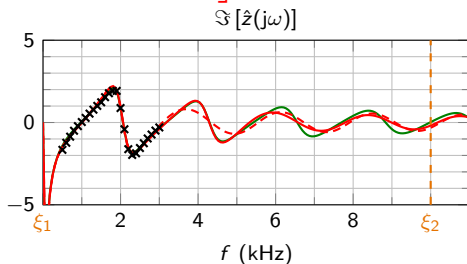
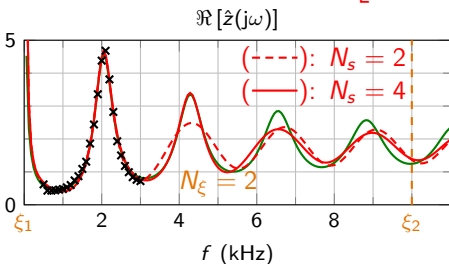
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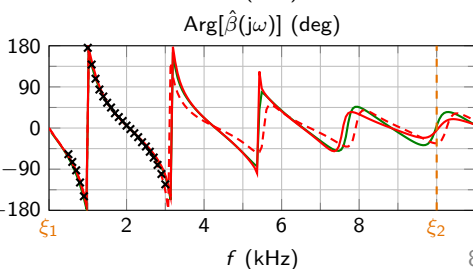
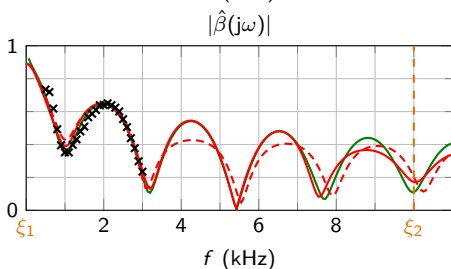
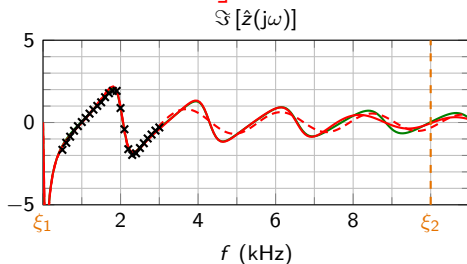
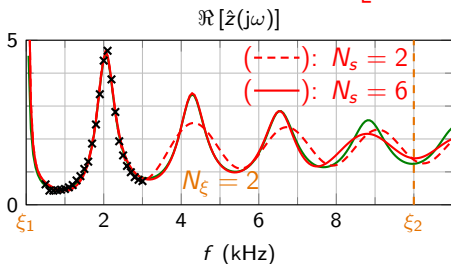
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Summary of Part I: Model analysis

Questions addressed in Part I

- (a) **Structure of physical impedance models?**
- (b) Well-posedness and stability?
- (c) **Discretization?**
- (d) Nonlinear absorption mechanisms?

Further results

- ① Characterization of OD kernels h
- ② Discretization of OD representation (quadrature method)
- ③ Application to other physical models \hat{z}_{phys} , \hat{y}_{phys} , $\hat{\beta}_{\text{phys}}$

⇒ Part II: Discretization with Discontinuous Galerkin

Part II: Objectives

Linearized Euler equations on $(0, T) \times \Omega$, $\Omega \subset \mathbb{R}^d$

$$\begin{cases} \partial_t p + (\mathbf{u}_0 \cdot \nabla) p + c_0 \nabla \cdot \mathbf{u} + \gamma p \nabla \cdot \mathbf{u}_0 = 0 \\ \partial_t \mathbf{u} + (\mathbf{u}_0 \cdot \nabla) \mathbf{u} + c_0 \nabla p + (\mathbf{u} \cdot \nabla) \mathbf{u}_0 + p(\mathbf{M}_0 \cdot \nabla) \mathbf{u}_0 = 0 \end{cases}$$

with IBC on $\Gamma_z \subset \partial\Omega$, $\mathbf{M}_0 = \mathbf{u}_0/c_0$.

Objective Discretization with Discontinuous Galerkin (DG) method

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Objective Discretization with Discontinuous Galerkin (DG) method

Continuous problem LEEs as Friedrichs system:

$$\partial_t \mathbf{v} + A(\nabla) \mathbf{v} + B \mathbf{v} = 0, \quad A(\mathbf{n}) = \begin{pmatrix} (\mathbf{u}_0 \cdot \mathbf{n}) \mathbb{I}_d & c_0 \mathbf{n} \\ c_0 \mathbf{n}^T & \mathbf{u}_0 \cdot \mathbf{n} \end{pmatrix}, \quad \mathbf{v} := \begin{bmatrix} \mathbf{u} \\ p \end{bmatrix}.$$

Semi-discrete problem $\partial_t \mathbf{v}_h + \mathcal{A}_h \mathbf{v}_h = 0$, where $\mathcal{A}_h : V_h \rightarrow V_h$ is

$$(\mathcal{A}_h \mathbf{v}_h, \mathbf{w}_h)_{L^2(\Omega)} := \sum_{T \in \mathcal{T}_h} \overbrace{(\mathcal{A} \mathbf{v}_h, \mathbf{w}_h)_{L^2(T)}}^{\text{weak formulation on } T} + \underbrace{\left((A(\mathbf{n}) \mathbf{v}_h)^* - A(\mathbf{n}) \mathbf{v}_h, \mathbf{w}_h \right)_{L^2(\partial T)}}_{\text{weak coupling}}$$

Outline

- 3 DG discretization of IBCs
 - Energy analysis
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Weak enforcement of IBCs

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⇒ Centered flux with ghost state \mathbf{v}^g

$$(A(\mathbf{n})\mathbf{v})^* := \frac{1}{2}A(\mathbf{n})\mathbf{v} + \frac{1}{2}A(\mathbf{n})\mathbf{v}^g, \quad \text{with } \mathbf{v}^g = \mathbf{v}^g(\mathbf{n}, \mathcal{Z}(\mathbf{v}), \mathbf{v}).$$

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The flux $(A(\mathbf{n})\mathbf{v})^*$ is said to be *admissible* if it is both consistent and passive.

- (Consistency) Let $\mathbf{v}(t) \in V$ be the exact solution.
- (Passivity) $\forall \mathbf{v}_h(t) \in V_h, t > 0,$

$$A(\mathbf{n})\mathbf{v}^g = A(\mathbf{n})\mathbf{v}.$$

$$\frac{1}{2} \int_0^t (A(\mathbf{n})\mathbf{v}_h^g, \mathbf{v}_h)_{L^2(\Gamma_z)} d\tau \geq 0.$$

+ desirable continuity conditions as " $\mathcal{Z}(\mathbf{v}) \rightarrow 0$ " or " $\mathcal{Z}(\mathbf{v}) \rightarrow \infty$ ".

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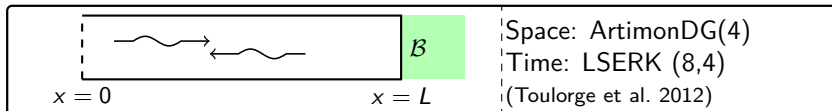
Results

- Consistent and unstable fluxes are possible
- 3 fluxes based on $\mathcal{Z}, \mathcal{Y}, \mathcal{B}$
- \mathcal{Y} may be preferable to \mathcal{Z}
- "Ideal": scattering operator $\mathcal{B} := (\mathcal{Z} - \mathcal{I}) \circ (\mathcal{Z} + \mathcal{I})^{-1}$

Outline

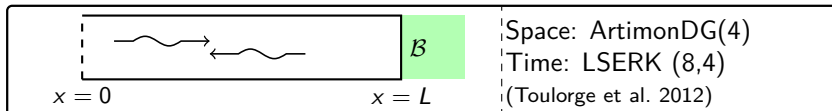
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Validation: nonlinear impedance tube



- Analytical solution even with nonlinear $\mathcal{B} \Rightarrow$ enables validation

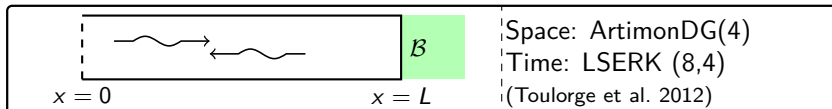
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Validation: nonlinear impedance tube



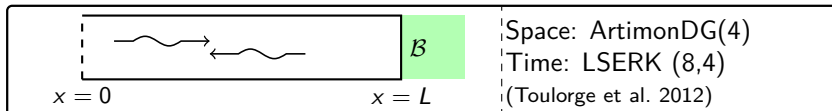
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$$\Rightarrow \mathcal{B}_C(v) \leq v.$$

Validation: nonlinear impedance tube

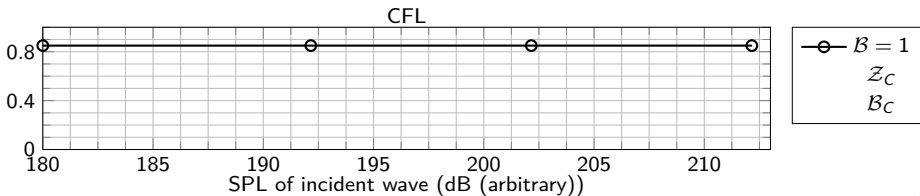


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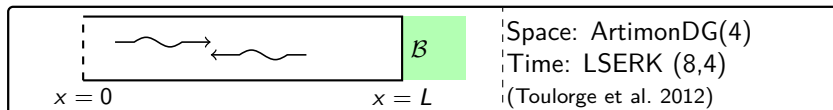
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$\Rightarrow \mathcal{B}_C(v) \leq v$. Differences between \mathcal{Z} and \mathcal{B} fluxes?



Validation: nonlinear impedance tube

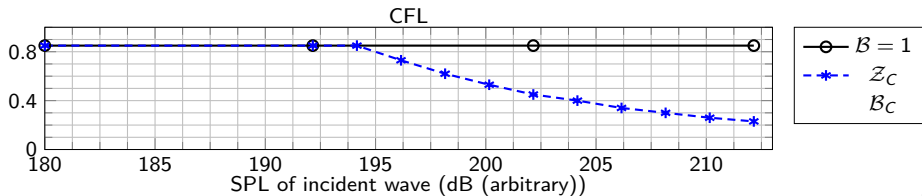


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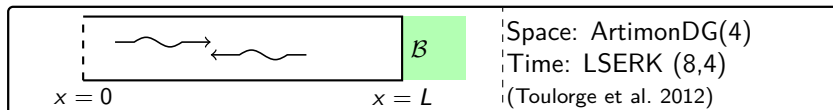
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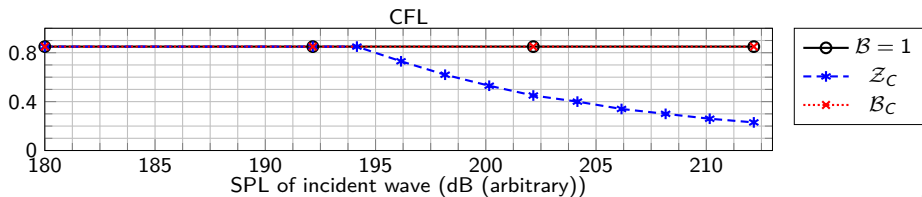


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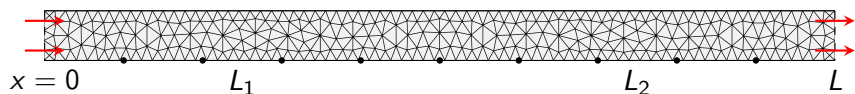
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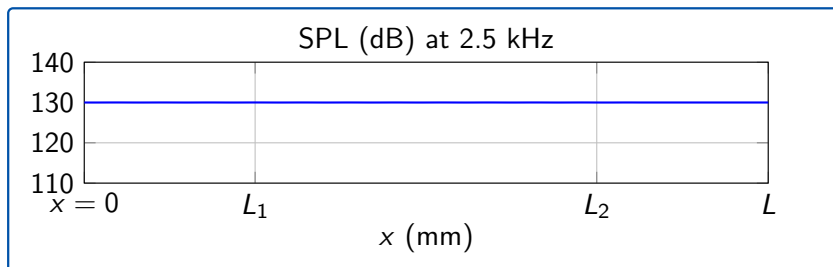
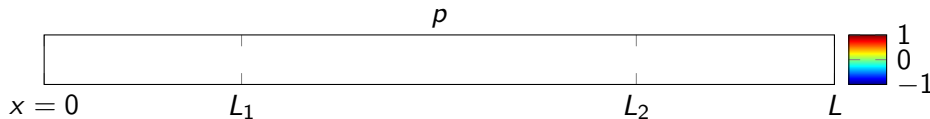
Outline

- 3 DG discretization of IBCs
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Aeroacoustical duct: overview

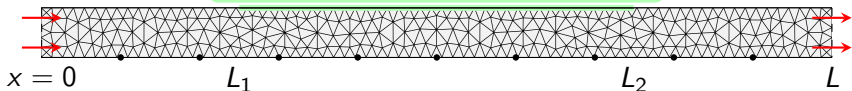


ArtimonDG(4). 552 triangles. CFL = 0.5. LSERK (8,4) (Toulorge et al. 2012)

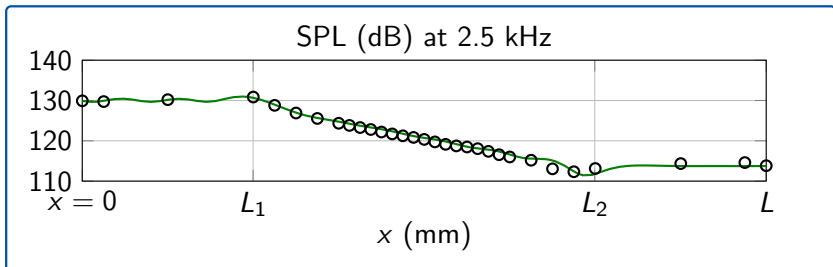
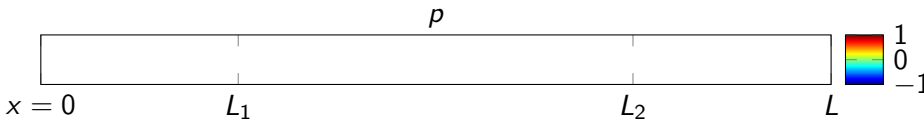


Aeroacoustical duct: overview

$\hat{\beta}_a(s)$ (liner CT57 – NASA Langley)

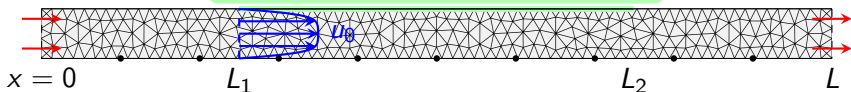


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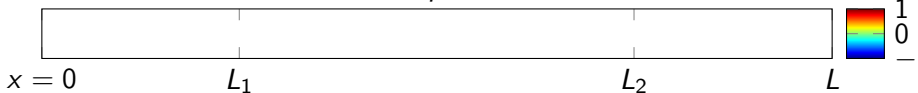
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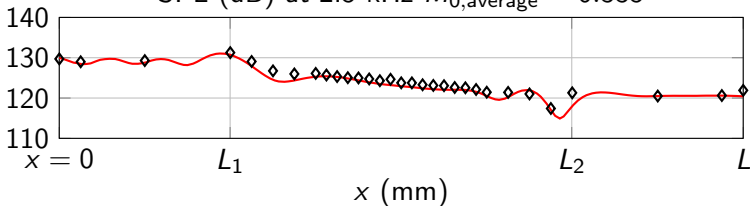


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ρ



SPL (dB) at 2.5 kHz $M_{0,average} = 0.335$



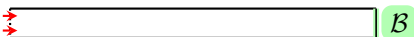
Summary of Part II: Discontinuous Galerkin discretization

Questions addressed in Part II

- (a) Structure of physical impedance models?
- (b) Well-posedness and stability?
- (c) **Discretization?**
- (d) **Nonlinear absorption mechanisms?**

Results

- ① Continuous, (Semi)-discrete energy analysis
⇒ Computational advantage of β, \mathcal{B} over z, \mathcal{Z}

- ② Numerical validation on impedance tube 

- ③ Numerical application in duct aeroacoustics 

⇒ Part III: Stability of wave equation with IBC

Part III: Well-posedness & Stability – Summary

Model analysis is useful in both theory and practice.

Principle Representation of $\hat{z}(s) \Rightarrow$ Cauchy problem on extended state

$$X = \overbrace{(p, u, \varphi, \psi)}^{\text{acoustic field}} \in \mathcal{H}.$$

additional variables

$$\frac{dX}{dt}(t) = \mathcal{A}X(t), \quad X(0) = X_0.$$

Objective What are we interested in?

Well-posedness and **asymptotic stability** of a strong solution X in \mathcal{H} .

Method of proof Spectral analysis of \mathcal{A} .

Asymptotic stability theorem: (Arendt et al. 1988; Lyubich et al. 1988).

Conclusions & outlook

Takeaways

(a) Structure of physical models?

- Admissibility using System theory
- Characterization of OD kernels h
- Application to physical models \hat{z}_{phys} , \hat{y}_{phys} , $\hat{\beta}_{\text{phys}}$

(b) Well-posedness and stability?

- Asymptotic stability of wave equation with positive-real IBC

(c) Discretization?

- Discretization of OD representation
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Outlook

- TDIBC for DDOF liners & “exact” acoustical models

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Outlook

- TDIBC for DDOF liners & “exact” acoustical models
- Computation of differential \mathcal{B}
- Nonlinear physical modeling
- Quadrature-based discretization of diffusive representations

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- Discretization of OD representation
- Computational advantage of β, \mathcal{B} over z, \mathcal{Z}
- Numerical application in duct aeroacoustics

(d) Nonlinear absorption mechanisms?

- Computation of algebraic \mathcal{B} and validation in nonlinear impedance tube

Outlook

- TDIBC for DDOF liners & “exact” acoustical models
- Computation of differential \mathcal{B}
- Nonlinear physical modeling
- Quadrature-based discretization of diffusive representations
- Stability of wave eq. with IBC
- IBCs with Euler or Navier-Stokes

Analysis and Discretization of Time-Domain Impedance Boundary Conditions in Aeroacoustics

Publications

F. Monteghetti et al. (2016). “Design of broadband time-domain impedance boundary conditions using the oscillatory-diffusive representation of acoustical models”. In: *The Journal of the Acoustical Society of America* 140.3, pp. 1663–1674. DOI: [10.1121/1.4962277](https://doi.org/10.1121/1.4962277)

F. Monteghetti et al. (2018b). “Energy analysis and discretization of nonlinear impedance boundary conditions for the time-domain linearized Euler equations”. In: *Journal of Computational Physics* 375, pp. 393–426. DOI: [10.1016/j.jcp.2018.08.037](https://doi.org/10.1016/j.jcp.2018.08.037)







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F. Monteghetti et al. (2018a). “Asymptotic stability of the multidimensional wave equation coupled with classes of positive real impedance boundary conditions”. (In revision.)

Thanks for your attention. Any questions?

Contact: florian.monteghetti@isae.fr

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